AMENDMENTS TO THE SPECIFICATION

Please replace paragraph number 0040 of the specification with the following paragraphs:

FIG. 21 shows another two-panel exemplary color projection system including skew ray depolarization compensation; ~~and~~

FIG 22 shows yet another two-panel exemplary color projection system including skew ray depolarization compensation; and

Please replace paragraph number 0053 with the following paragraph:

As the number of layers is increased to address the spectral criteria, the total retardance of the stack can rise to well over 10,000 nm. The composite structure can be considered the combination of a composite or compound retardation and rotation at each wavelength, as described by a Jones' matrix. While the network synthesis technique ("NST") identifies numerous stack designs that provide the same power spectrum, each has a unique Jones' matrix. (The ~~network synthesis technique~~ NST (see Harris et al. (1964), J. Opt. Soc. Am. 54:1267, Ammann et al. (1966), J. Opt. Soc. Am. 56:1746, and Ammann (1966), J. Opt. Soc. Am. 56:943) is a procedure for determining the orientations of the N retarders, and the exit polarizer, to obtain the desired amplitudes of the (N+1) impulses.) A common characteristic is that a stack has a significant compound retardation with a fairly stable eigenpolarization along the direction of the design axis. This retardation is often characterized by fairly linear phase within the flat regions of the spectrum. Typically, the retardation in the converted band differs from that in the non-converted band. Nonlinear phase often exists in the transition band of the spectrum.

Please replace paragraph number 0059 with the following paragraph:

In general, the network synthesis method does not identify structures that provide zero compound retardation. Evaluating the Jones' matrix of each design can identify structures with the lowest compound retardation. Further reduction in compound retardation can be accomplished by placing a bias retarder parallel/perpendicular to the design axis according to the present invention. The bias retarder is crossed with the compound retarder of the stack, with retardation selected to minimize the net retardance. This is done with no impact on the spectrum along the design axis. The bias retarder can either ~~proceed~~ precede or follow the stack, with unique results in each case. Moreover, a different bias retardance on either side of the stack may be used to optimize results. If the bias retarder(s) can be well matched to the stack, then the structure satisfies that Case 1 criterion.

Please replace Table 1 on page 11 with the following table.

TABLE 1		
	Non-rotated band	Rotated band
CASE 1 - parallel reflecting planes – as shown and described in Figure 12 and its accompanying text.	$\begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$ Identity. Does nothing since there is no need to alter the polarization state of any rays. There is no mixing of polarization states since PBS axes are parallel for all rays.	$\begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}$ Pure 90° rotation. Any input polarization axes will be rotated by $\pi/2$ regardless of input polarization.
CASE 2 – perpendicular reflecting planes– as shown and described in Figure 11.	$\begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}$ Reflection about axes defined by normally incident ray polarization.	$\begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix}$ Reflection about axis bisecting orthogonal axes, one of which is defined by normally incident ray polarization.